

COMBINED LOADING OF BURIED THERMOPLASTICS PRESSURE PIPES

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Introduction

Combined loading test

Results

Conclusions

EN805 “Water supply-Requirements for systems and components outside buildings”

demands product standards to

“State the relationship between product pressure classification (PN) and Operational pressure (PFA)”

Proposed approach with thermoplastics (see also EN1401)

$$PFA = fa * ft * PN$$

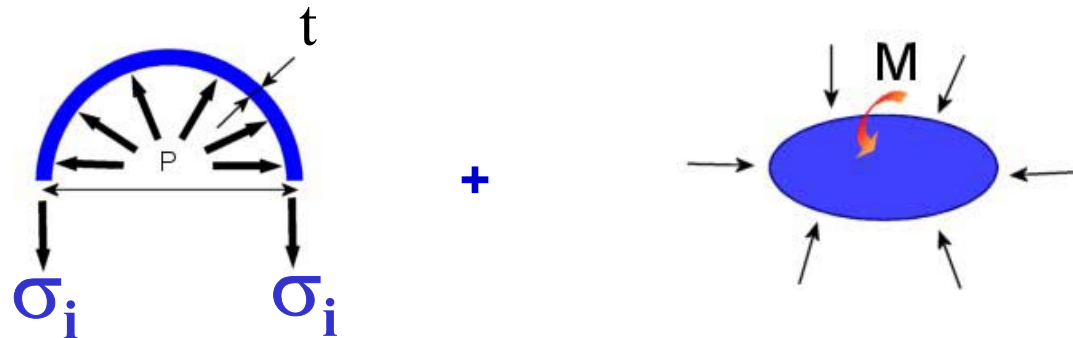
PN = Pressure rating of product

ft = Temperature rating factor

fa = Application rating factor

Introduction: Traditional (materials) design

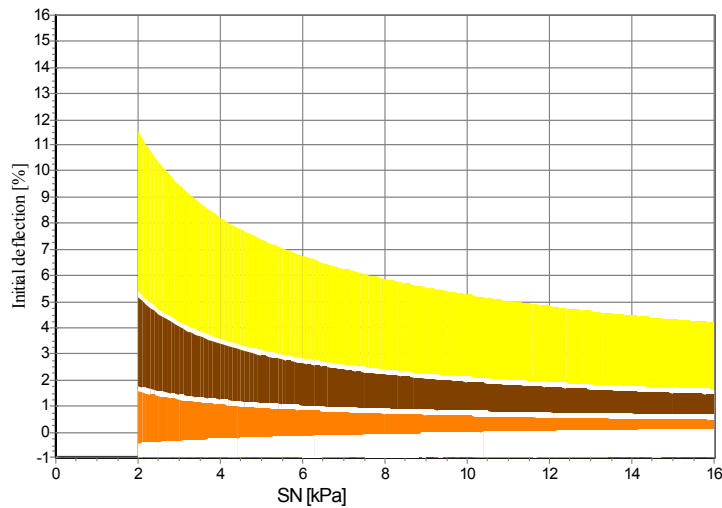
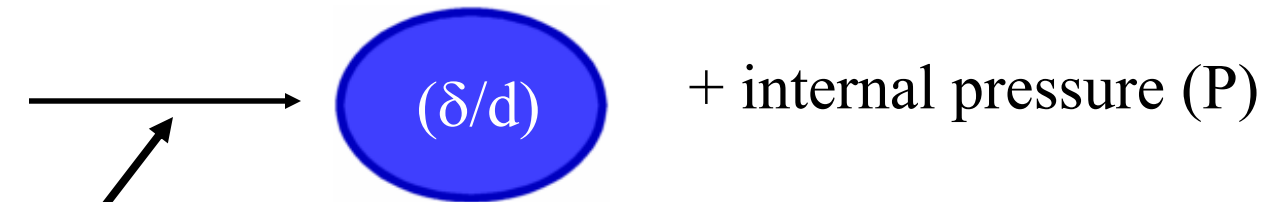
Stress = Stress from internal pressure + Stress from external load



$$(MRS / C =) \quad HDS = \quad PFA / 2 * (SDR-1) \quad + \quad ? \quad M / W$$

Loading condition:

- depth
- soil
- traffic
- SN
- Installation



$$PFA = fa * PN$$

CEN TC164/165 JWG1 TG2

“defined 9 loading conditions to which to refer to in the product standard”

Case	fa
1	1
2	0.9 ? etc
3	..
4	..
5	..
6	..
7	..
8	..
9	..

Analytical / numerical analysis

geometrical modeling

material modeling

creep

relaxation

Experimental analysis

test methods delivering

similar to practice

situations.

Deflected pipe test

Deflected pipe test



Note: Test does not allow re-rounding

2-6-2008

1. Pipe deformed to x% deflection
Stress relaxation starts
2. Internal pressure applied
Sustained load = creep
3. Measure the time to failure
4. Ratio=Failure time_x%/ failure time_0%

$$\varepsilon = 4.28 * (\delta/d) * (s/d)$$

$$\sigma (t) = [E / (1-\nu^2)] * \varepsilon * t^{(-m)}$$

$$\sigma_{\text{crown}} = P (d-\delta-2s)/(2*s)$$

$$\sigma_{\text{springline}} = P (d+\delta-2s)/(2*s)$$

Deflected pipe test: Test program

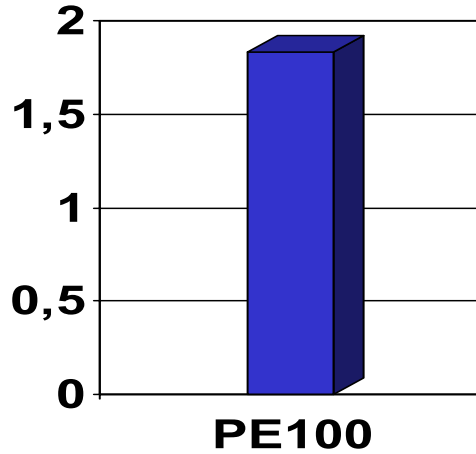
<i>Material</i>	<i>Stress</i>	<i>Temperature</i>	<i>Deflections</i>
PE100	12.5	20	0 & 8
PE80 standard	5.9	80	0 & 5 & 10
PE80 type 1	4.5	80	0 & 5 & 10
PE80 type 2	4.0	80	0 & 5 & 10
PVCO	26.0	60	0 & 5 & 10

Deflected pipe test: Test program

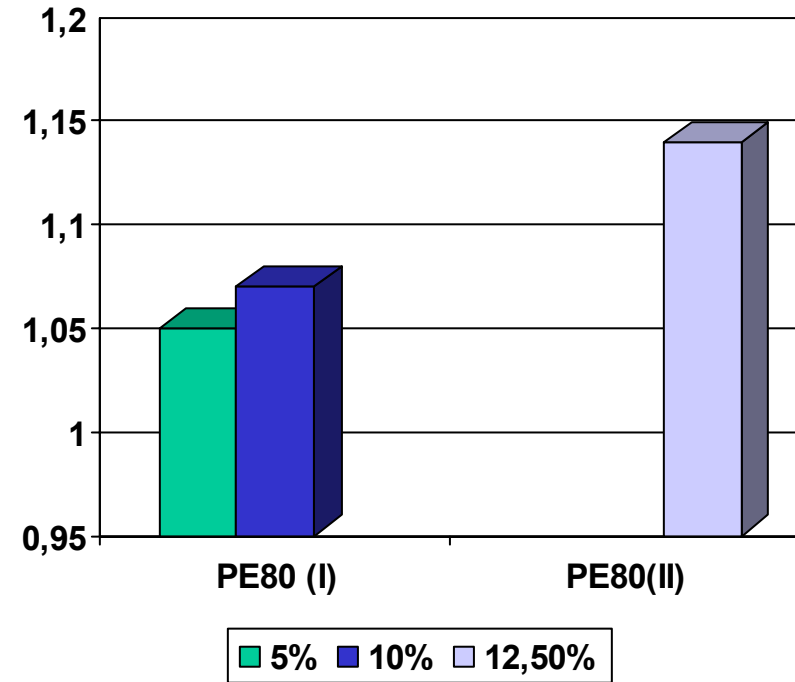
<i>Material</i>	<i>(δ/d) [%]</i>	<i>Ratio $t_{(\delta/d)} / t_{(0)}$</i>	<i>Failure type</i>
PE100	8	1.83	ductile
PE80 standard	5	616	ductile
	10	647	ductile
PE80 type 1	5	1.05	brittle
	10	1.07	brittle
PE80 type 2	12.5	1.14	brittle
PVCO	5	4.14	ductile
	10	8.73	ductile

Results deflected pipe test.
Value below 1 then effect; value=1 then no effect;
value>1 then positive effect

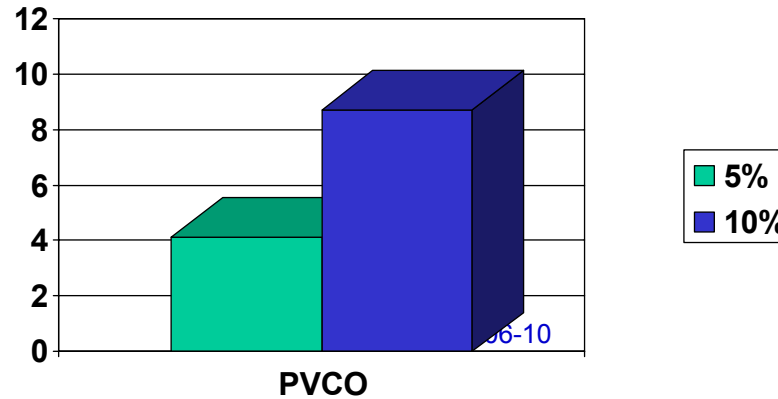
PE100 ductile
20 C



PE 80, brittle failures
80 C



PVCO, ductile
60 C



Concluding remarks deflected pipe tests

Pipes failing in a ductile manner profit from combined loading

Pipes failing in a brittle manner are not affected by combined loading

The free creep condition (as with material classification) is the worst condition

In an actual buried situation this condition refers to pipes installed in weak soils like peat.

Hence:

$$PFA = PN = 2 \cdot HDS / (SDR-1)$$

'Bicycle' test

Combined loading by axial bending

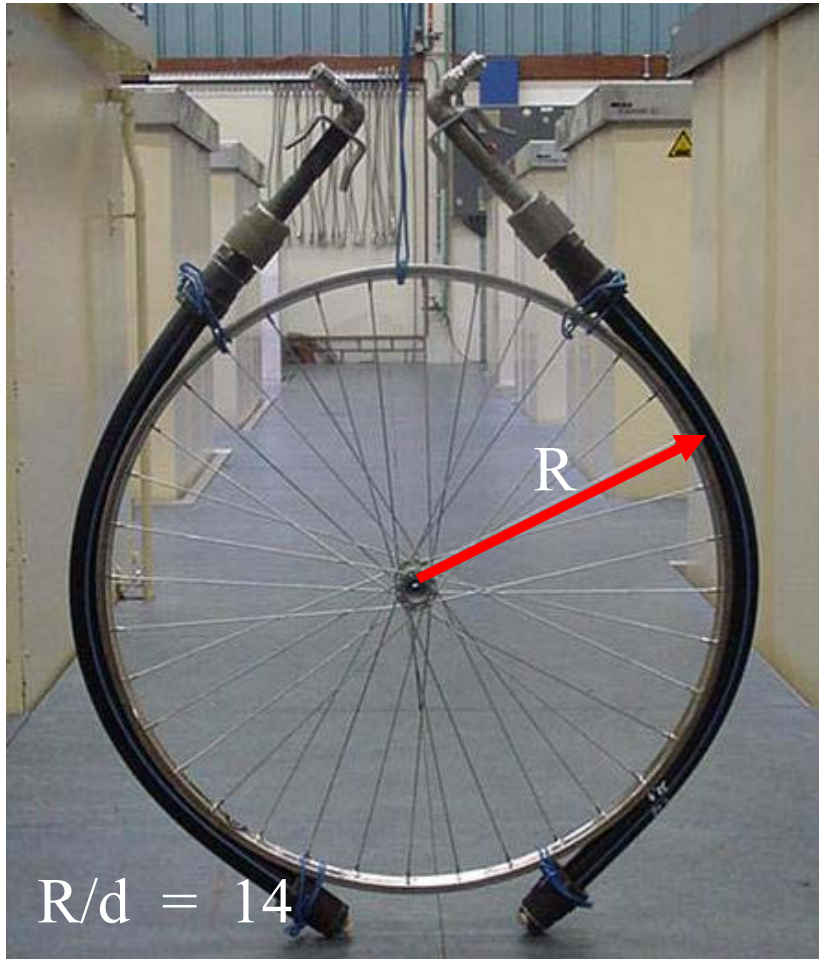
Prof. Wintergerst (1973)

Axial bending

Ring deflection

+

Internal pressure



Note: Test allows re-rounding

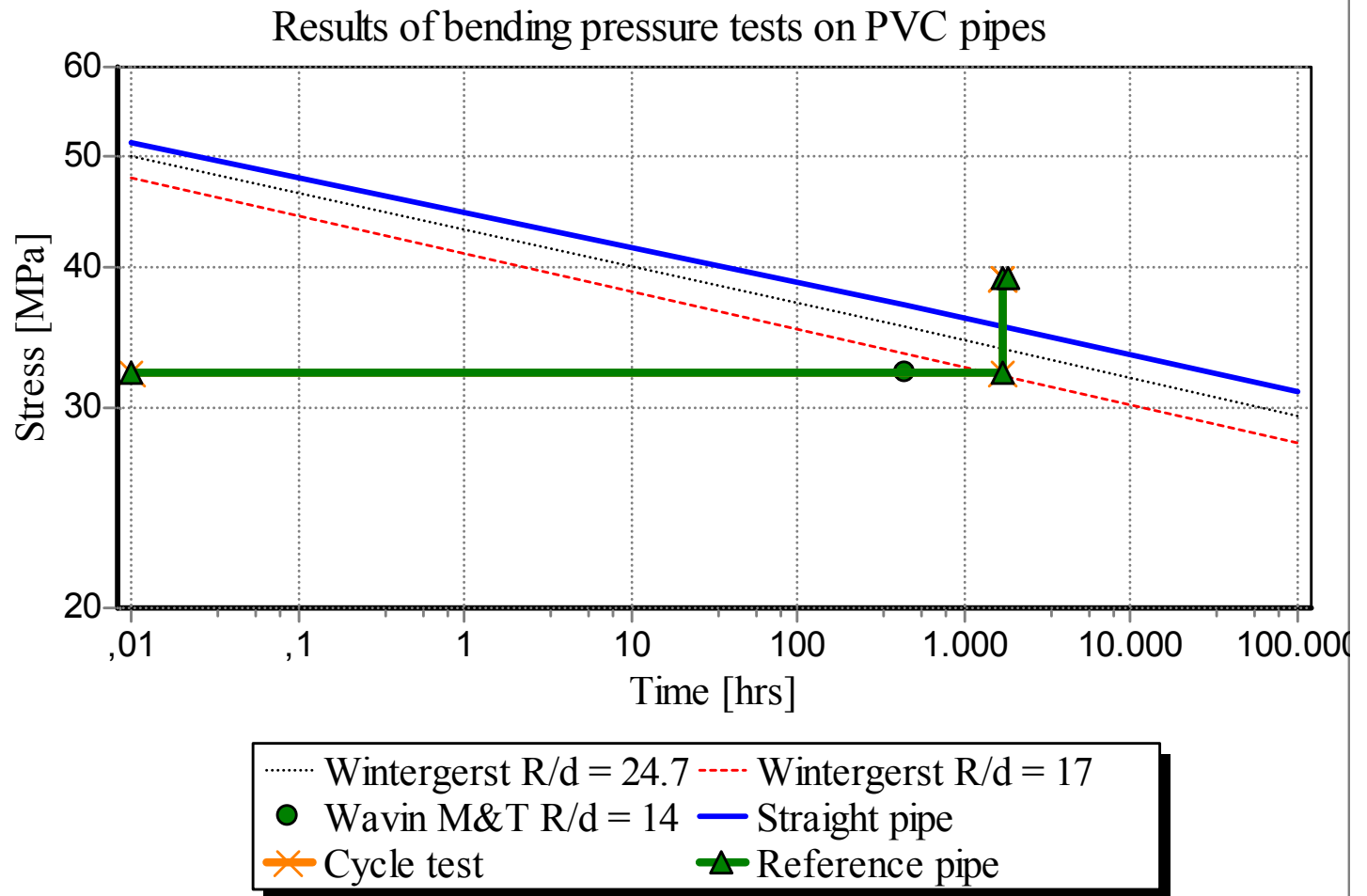
1. Pipe bend to fixed radius
Stress relaxation starts
2. Internal pressure applied
Sustained load = creep
3. Measure the time to failure

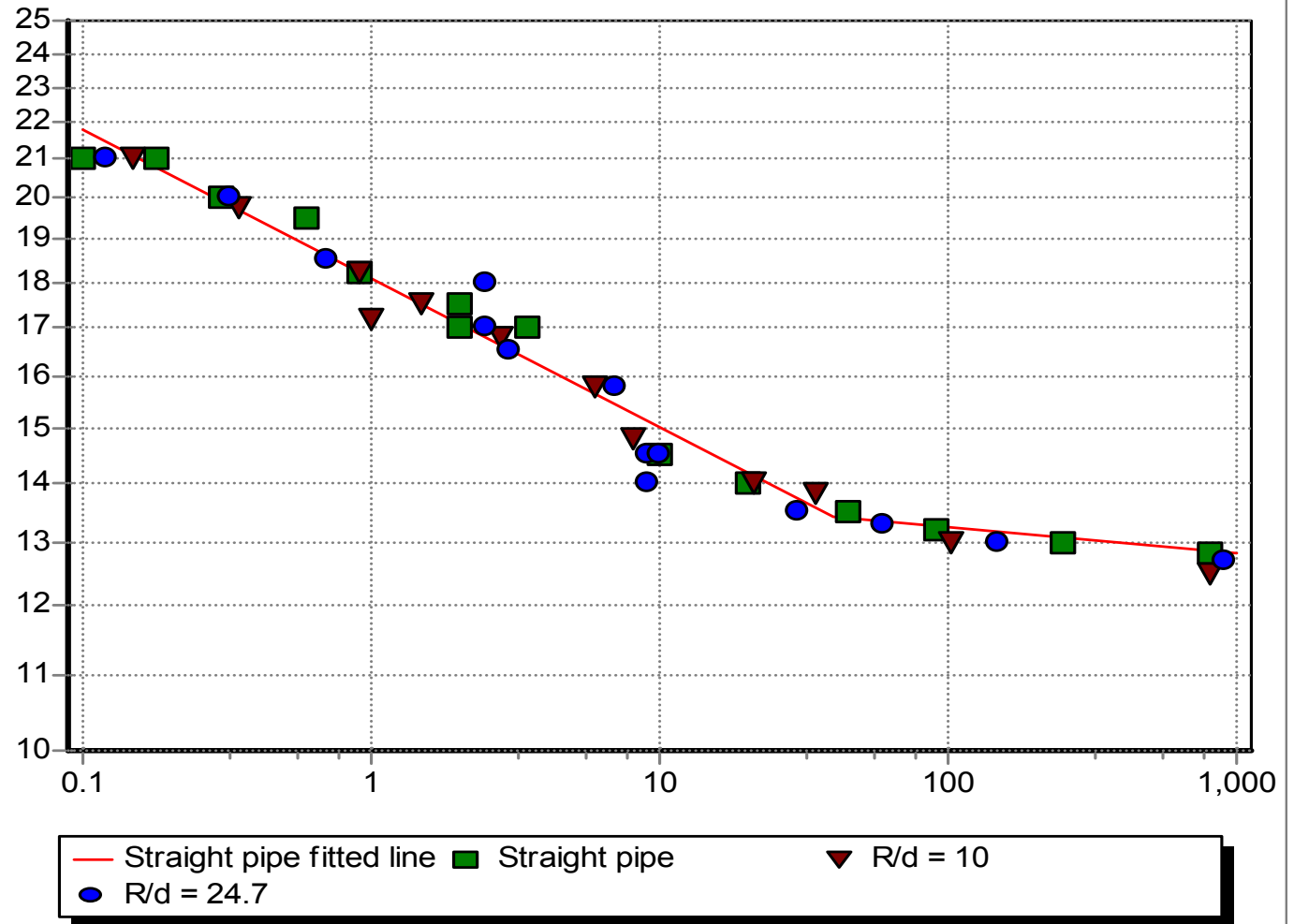
$$(\delta/d) = 1/16 * (d/s)^2 * (D/R)^2 * (1-v^2)$$

$$\epsilon_0 = 3 * (\delta/d) * (s/d)$$

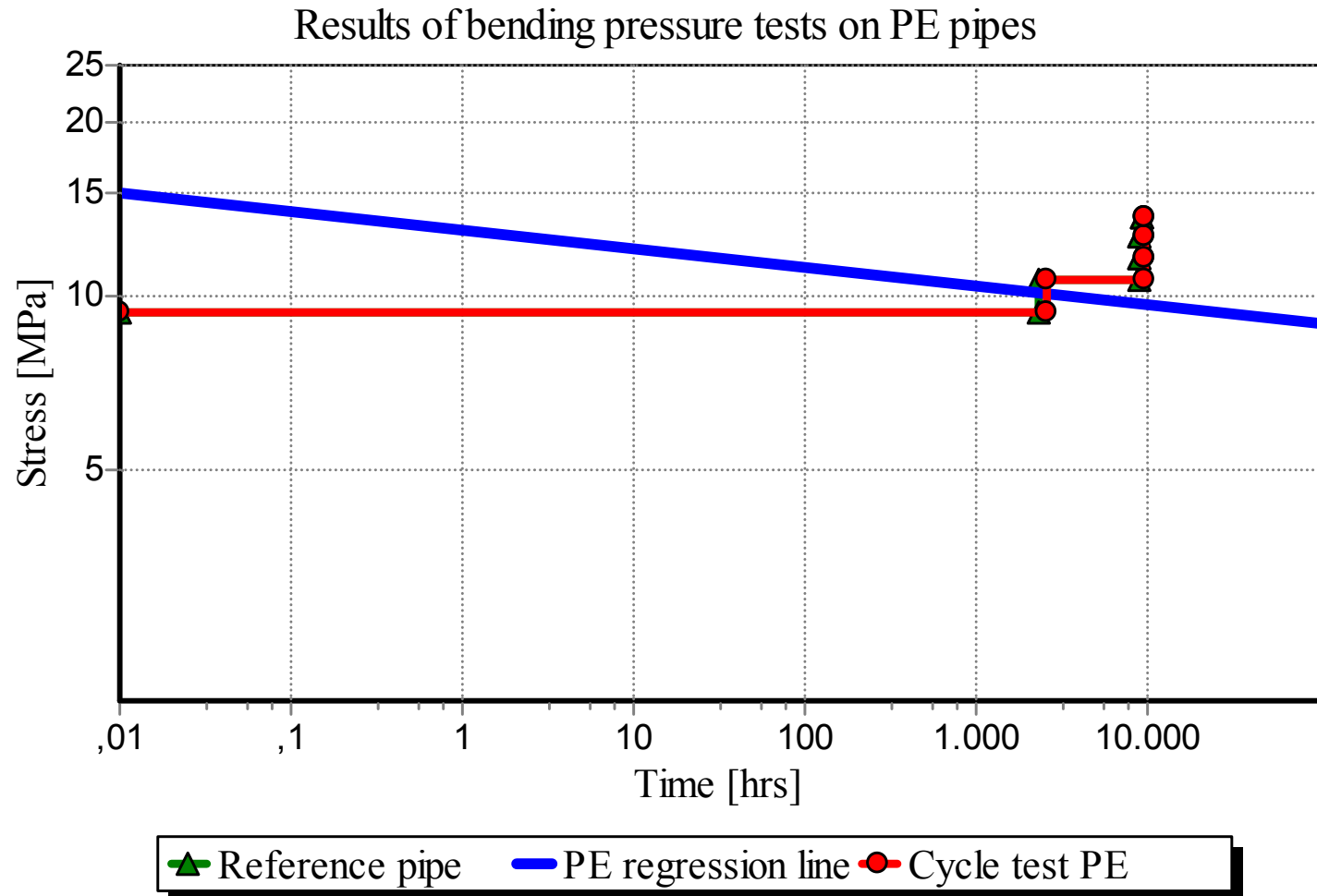
$$\epsilon_{ax} = (D - ((\delta/d) * d) / 2) / (2 * R)$$

Material	R/d	Temperature	Stress [MPa]
PVC	14	20	32.2 - 39.1
PE80	11	20	9.6-13.6
	11	80	3.94 - 4.6

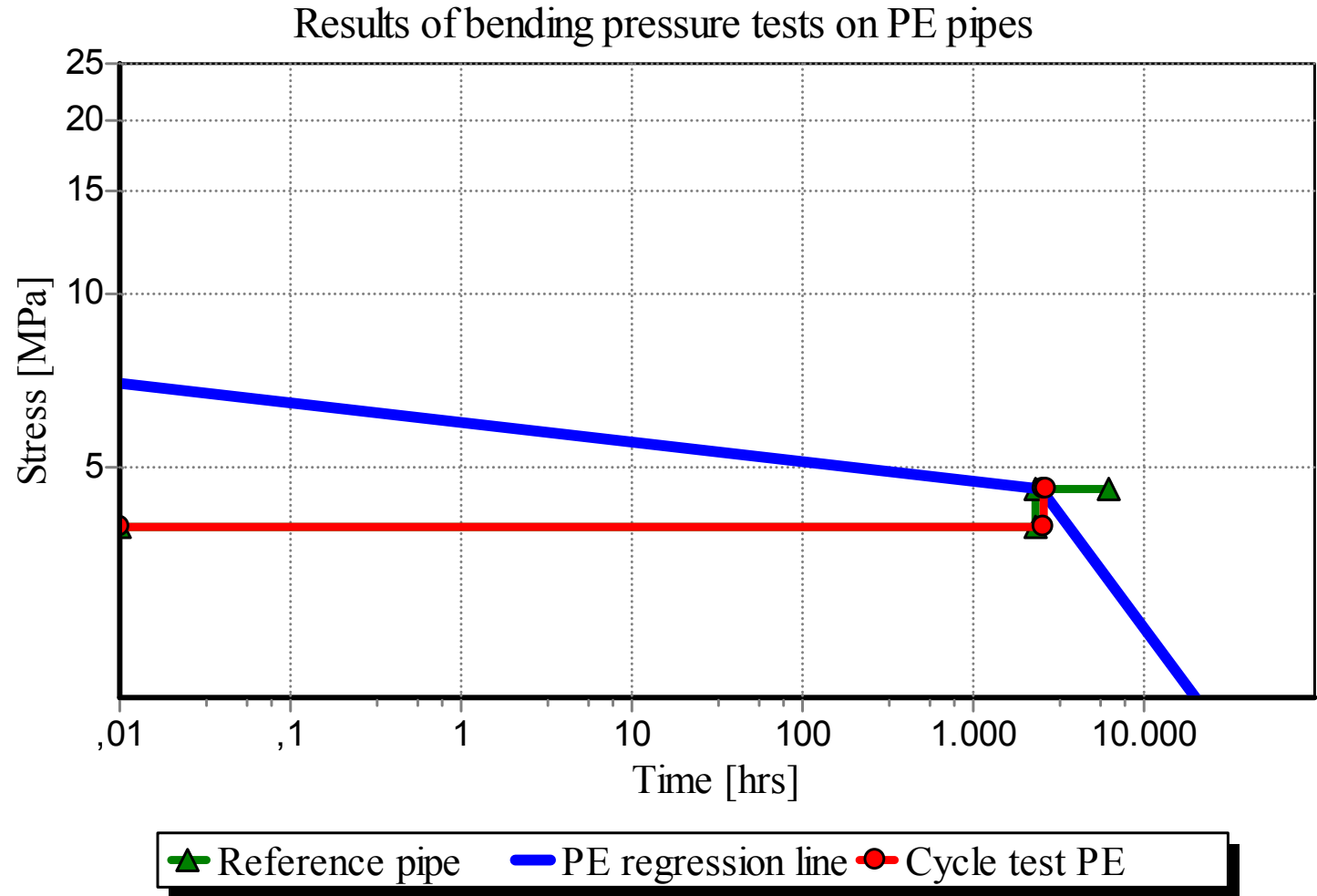




Results PE at 20 °C, ductile failures



Results PE 80 °C , brittle failures



$$PFA = f_a * f_t * PN$$

f_t = material dependent, but only an issue when $T > 20 \text{ }^\circ\text{C}$

$f_a = 1$ under condition that:

$$(\delta/d) < 12.5 \%$$

Bending radii

$$R > 50*d$$

The authors like to acknowledge

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CEN TC155 AHG40
“Design related material properties”